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Deformation and Failure in Dentin: A Mechanistic and Fracture Mechanics Based Approach

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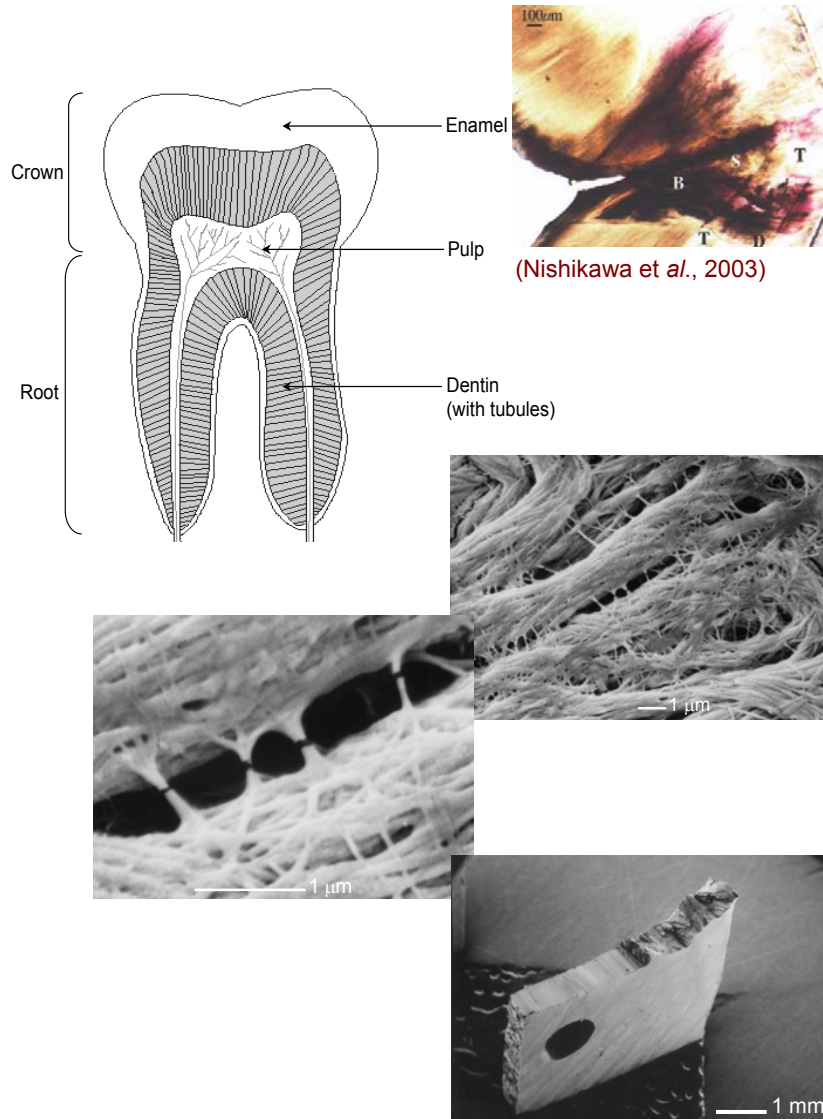
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Motivation and Significance



- Dentin is the most abundant mineralized tissue in teeth, and is critical for structural integrity
- Fracture and fatigue properties of dentin are an issue of obvious clinical relevance
- Non-carious notches in exposed root surfaces are sites for fracture and fatigue cracking
- Very few *fracture mechanics* based studies reported in archival literature
- Mechanical properties of dentin have implications for other mineralized tissues, such as bone



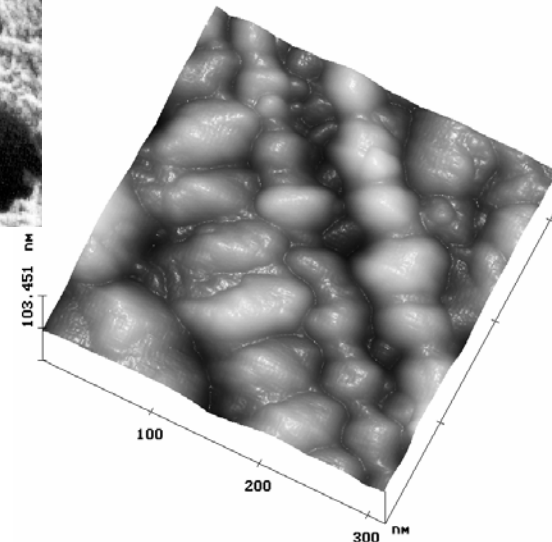
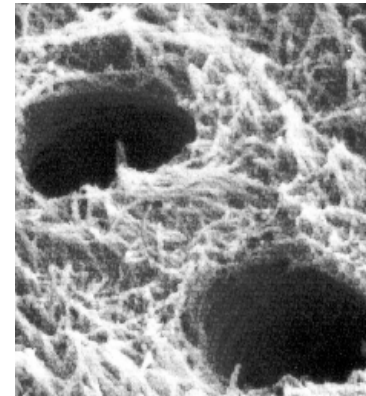
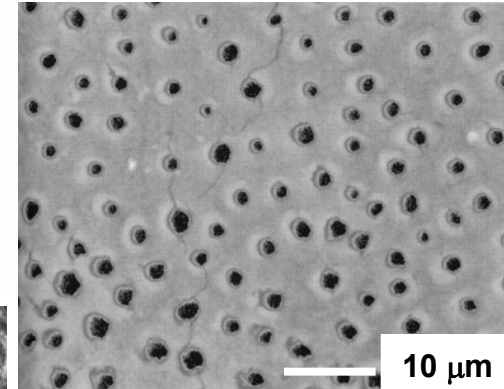
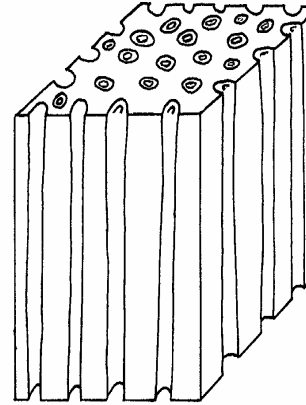
Objectives



- Measure the mechanical properties, specifically fracture toughness, fatigue and subcritical crack-growth properties, of dentin, as a function of orientation
- Characterize the micro-mechanisms of fracture in terms of the underlying features, and anisotropy, of the microstructure
- Identify and model the salient toughening mechanisms in dentin
- Establish a mechanism for the fatigue of dentin
- Develop a physical basis for a damage-tolerant life-prediction methodology for teeth

Microstructure of Dentin

- Distinctive features are 1-2 μm dia. cylindrical **tubules**, running from the dentin-enamel junction to the soft, interior pulp
- Hydrated composite of nanocrystalline carbonated apatite mineral (~45% vol.), collagen fibrils (~30% vol.) and fluid (~25% vol.)
- Mineral **crystallites** (5 nm thick) distributed in a scaffold of **collagen fibers** (50-100 nm dia.)
- Collagen fibrils form a planar felt-like structure oriented perpendicular to the tubules
- A simplified model for other mineralized tissue, such as bone?





Fracture and Fatigue of Dentin: Objectives



- What is the *macroscopic* fracture toughness of dentin?
- What is the *local* criterion for fracture in dentin?
- Does the highly directional nature of the microstructure affect the toughness and crack growth?
- Mechanistically, what are the origins of toughness in dentin?
 - What effect do the tubules have, either by blunting or deflecting cracks?
 - Can the collagen fibrils promote crack bridging?
 - Are there other salient toughening mechanisms?
- What is the nature of inelasticity (“yielding”) in dentin?
- What is the nature of fatigue and cyclic damage in dentin?

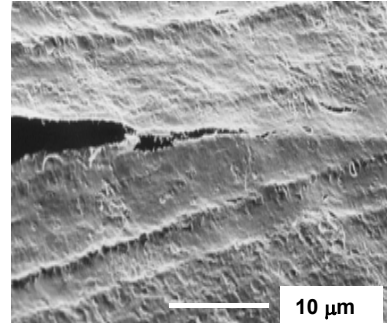
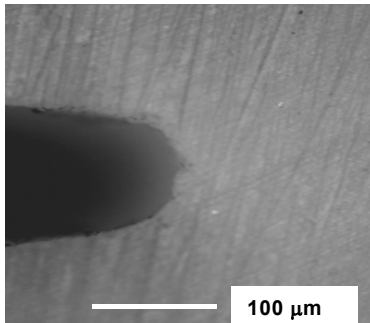
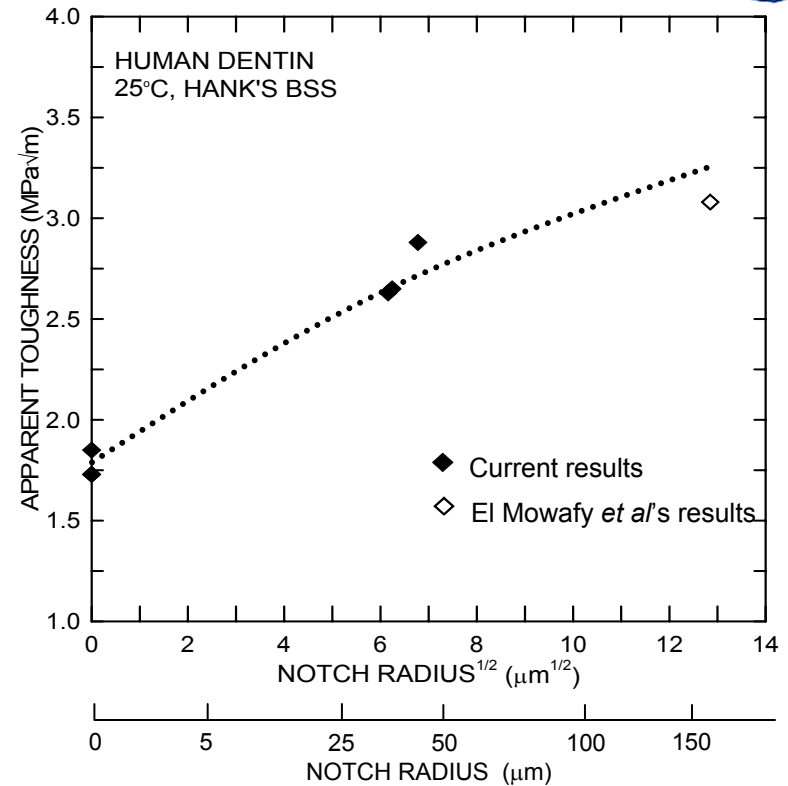
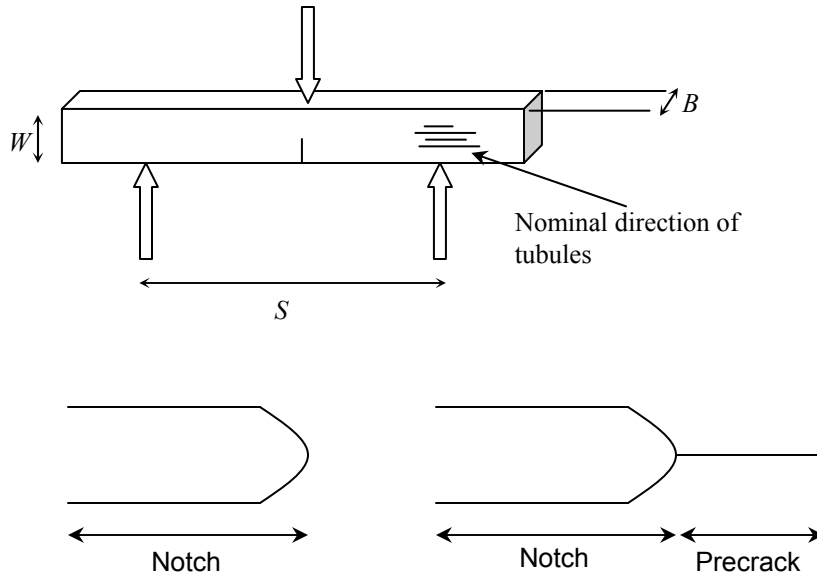


Fracture Toughness of Dentin



- Rasmussen *et al.*, (1976 & 1984)
 - first study of the toughness of dentin approach
 - found an orientation dependence on toughness – material was tougher parallel to tubules than perpendicular to tubules
 - toughness was measured by “work of fracture”; results are size and geometry dependent
- el Mowafy *et al.*, (1986)
 - first fracture-mechanics based study - using C(T) samples
 - measured $K_c = 3.08 \text{ MPa}\sqrt{\text{m}}$ for fracture parallel to tubules
 - overestimate of toughness as notched, not precracked, sample used
- Ruse *et al.*, (2001)
 - used so-called “Notchless Triangular Prism” technique
 - reported orientation-dependent values of $K_c = 1.13 - 2.02 \text{ MPa}\sqrt{\text{m}}$
 - non-standard test configuration

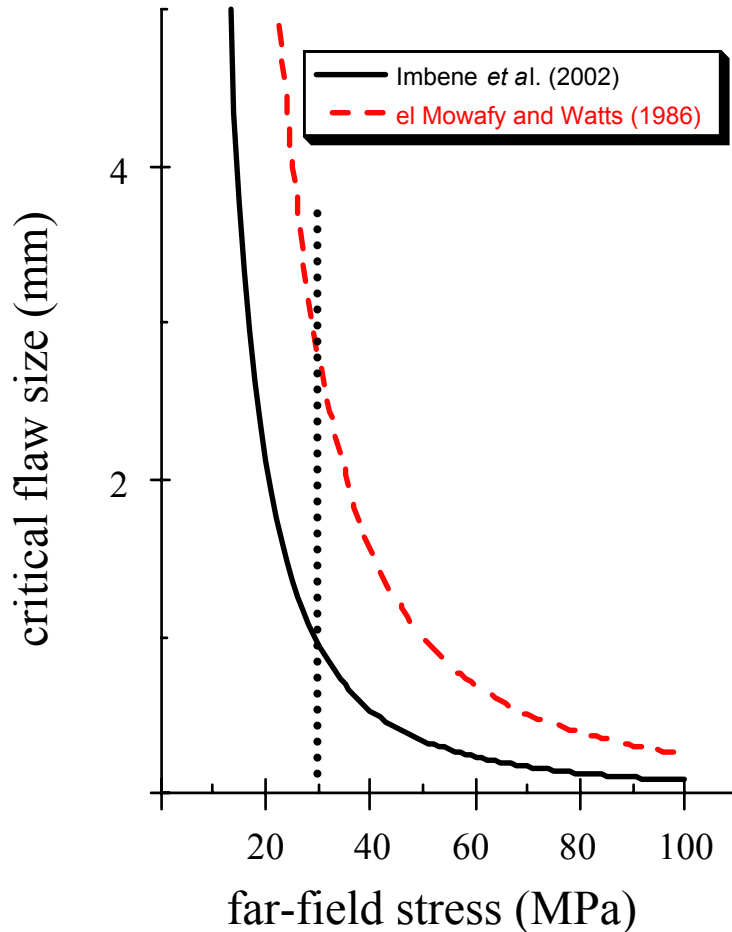
Fracture Toughness – Notch vs. Precrack



Definite effect of precrack acuity on K_{IC} :

- Notch toughness = 2.7 MPa√m (s.d. 0.1)
320 J/m² (s.d. 0.4)
- Precrack toughness = 1.8 MPa√m (s.d. 0.1)
140 J/m² (s.d. 0.4)

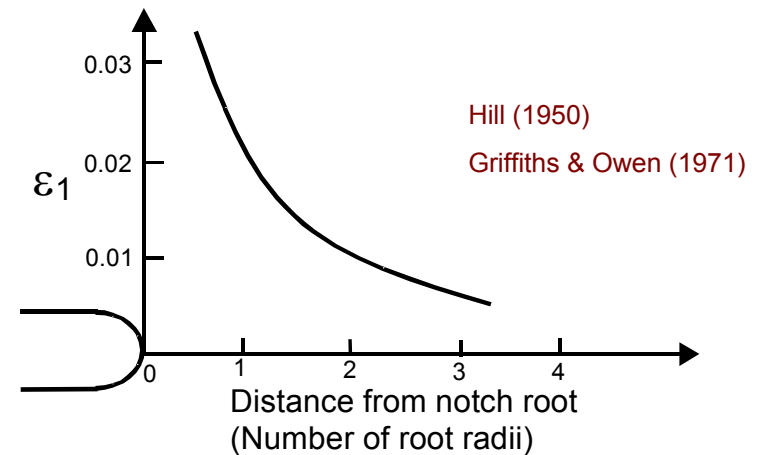
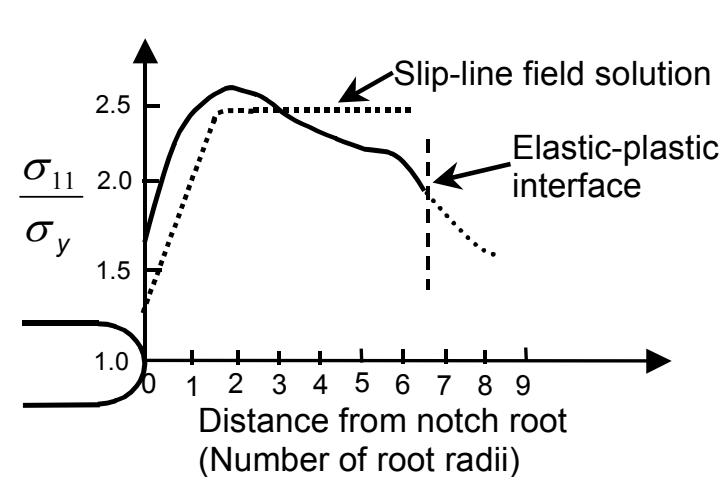
Estimation of Critical Flaw Sizes



- Lower estimate of $K_c < 2 \text{ MPa}\sqrt{\text{m}}$ significantly reduces the critical flaw size in dentin
- For comparison:
 - dental cements $K_c \sim 0.1\text{-}0.5 \text{ MPa}\sqrt{\text{m}}$
 - amalgams $K_c \sim 0.1\text{-}1.6 \text{ MPa}\sqrt{\text{m}}$
 - dental composites $K_c \sim 0.6\text{-}2.0 \text{ MPa}\sqrt{\text{m}}$
- However, catastrophic fracture is not the only problem - subcritical crack growth, e.g., by fatigue, is also an issue
- Life prediction based on time (or cycles) for flaws to grow subcritically

Stress- vs. Strain-Controlled Fracture

- Fracture of mineralized tissue invariably modeled as *strain-controlled*
- However, there is no experimental support for this hypothesis

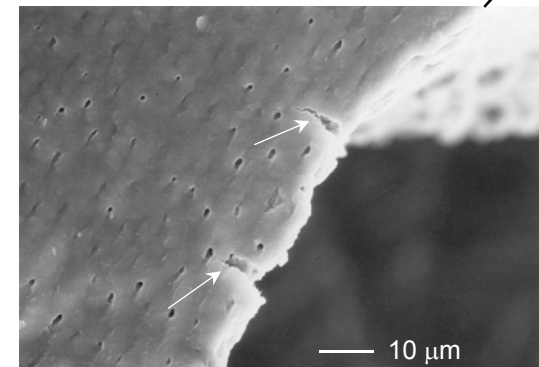
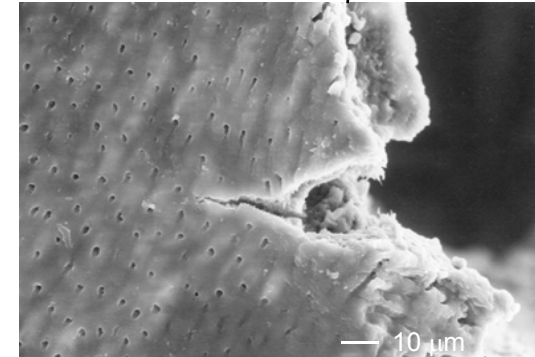
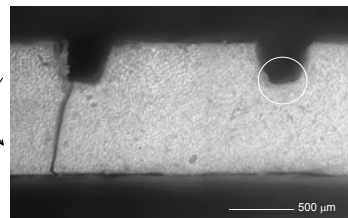
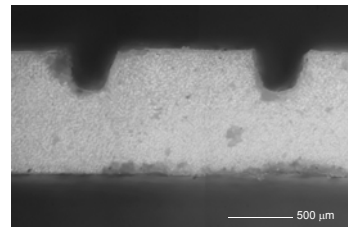
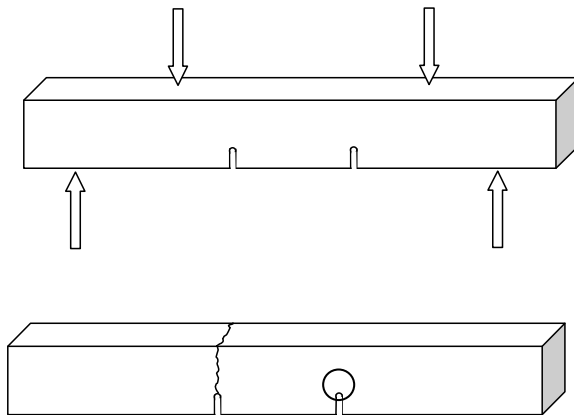


For fracture at a notch in a material displaying some degree of inelasticity

- **stress-controlled fracture:** initiates *ahead* of the notch
- **strain-controlled fracture:** initiates *at* the notch

Double-Notch Four-Point Bend Test

- Two identical notches in a four-point bend bar
- Constant bending moment on both notches
- One notch breaks - the other *freezes* local microstructural events just prior to fracture
- A good way to obtain stable cracks in dentin

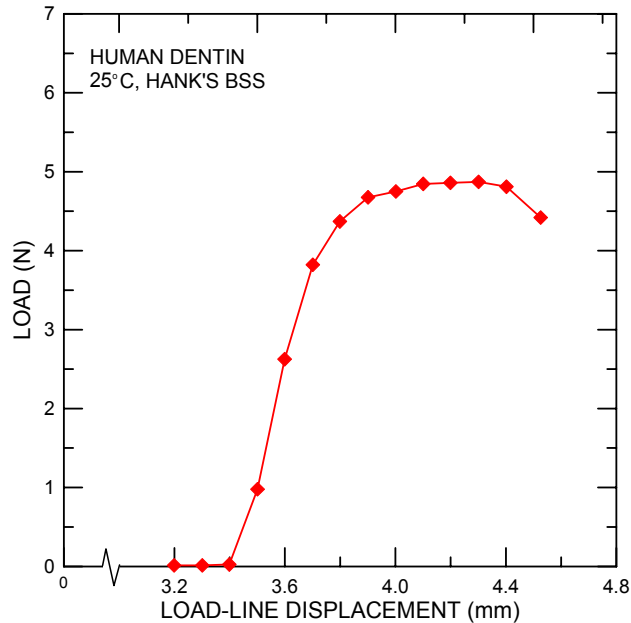


Notch
surface

- Crack initiation directly *at* the notch root provides definite evidence that fracture in dentin is ***strain-controlled***

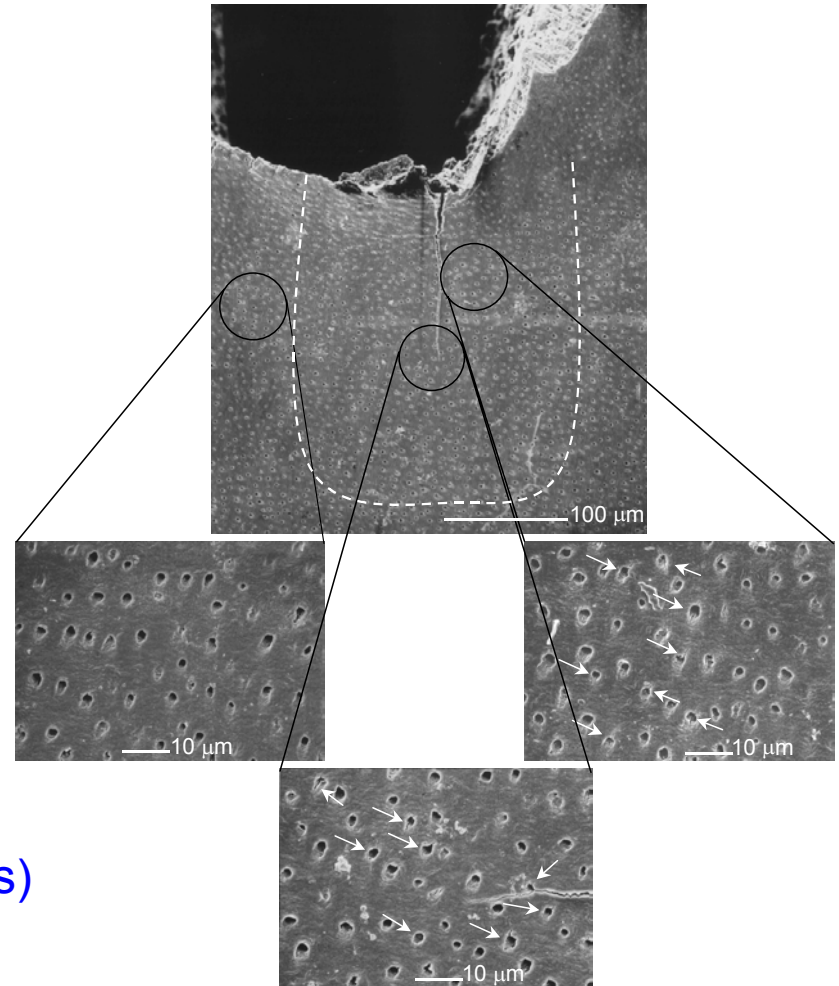
Nature of Inelasticity in Dentin

- uniaxial tensile test



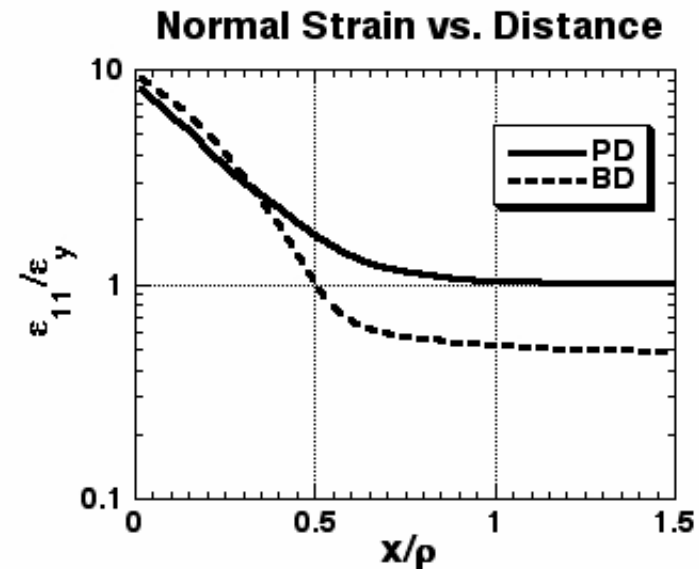
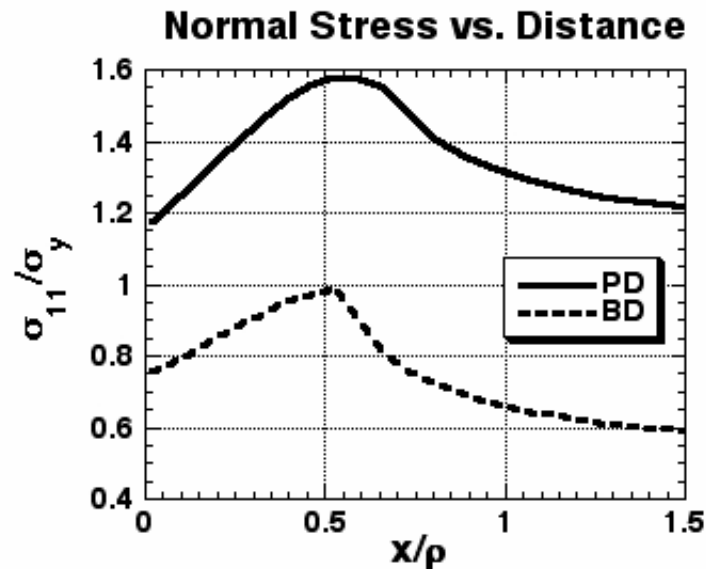
Inelastic deformation results from:

- plastic deformation (in the collagen fibrils)
- microdamage (at the peritubular cuffs)
- poro-elasticity (from fluid in the tubules)

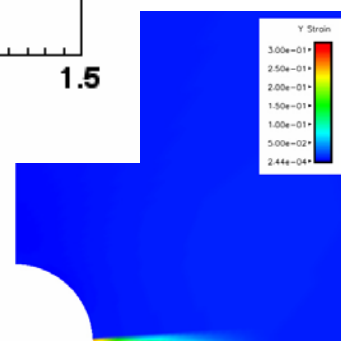
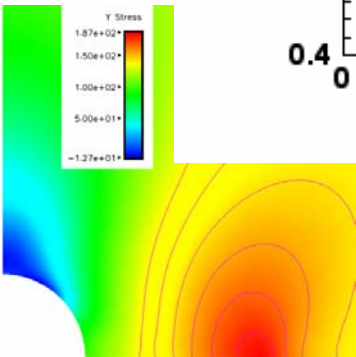


Plastic Damage vs. Brittle Damage

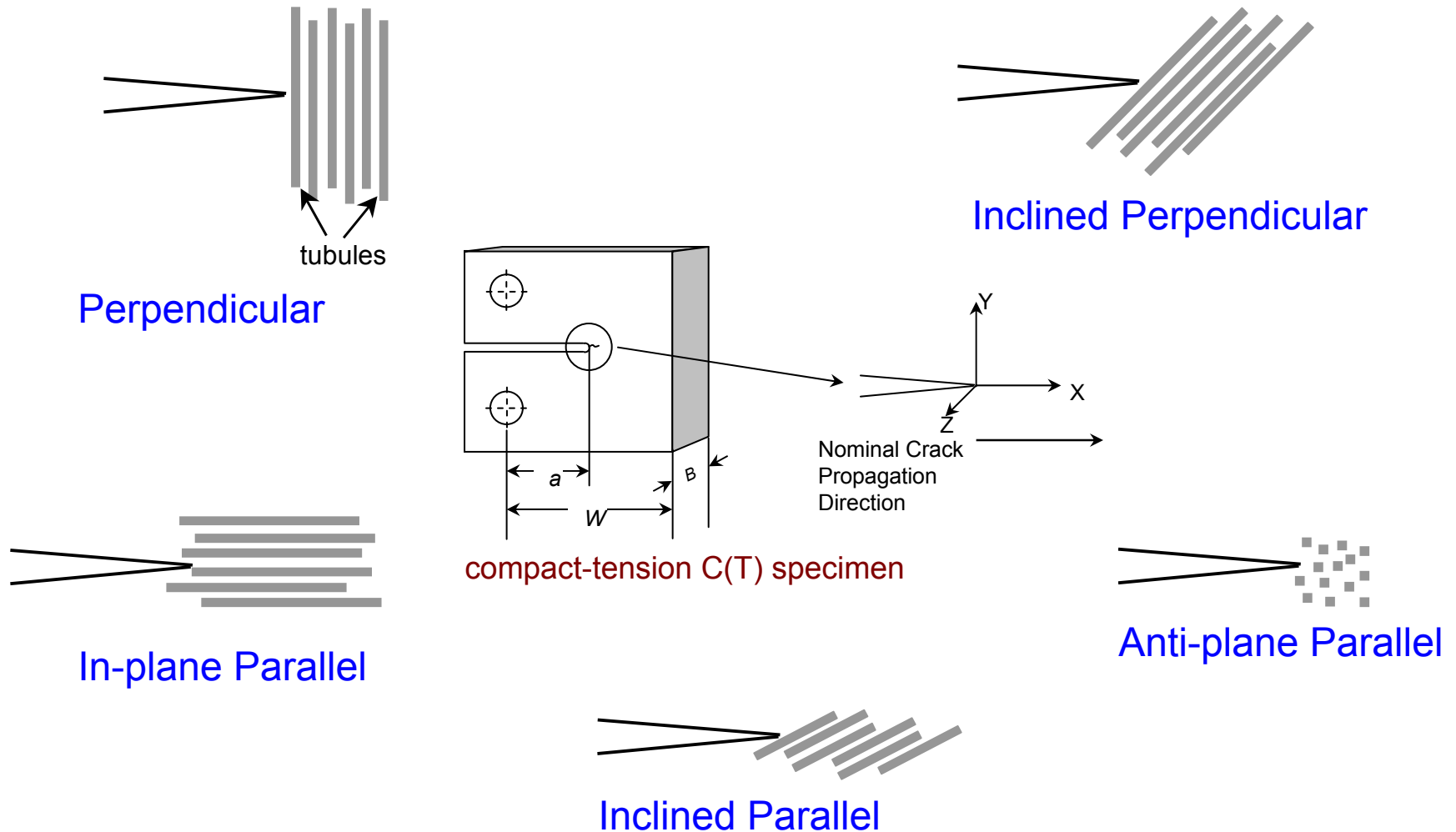
- Finite element simulation, using NIKE3D, of deformation by **plasticity**, using *Plastic Damage (PD) model* (Niebur et al., 2000), and **microcracking**, using *Brittle Damage (BD) model* (Govindjee et al., 1995)
- For both pressure-insensitive plasticity and pressure-sensitive microcracking, notch-field stress and strain distributions are *qualitatively* similar



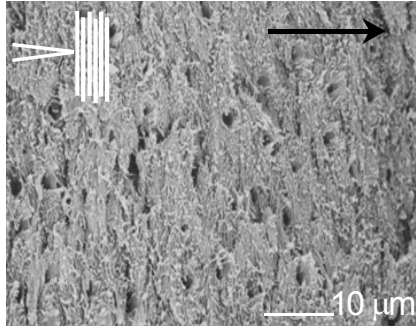
Distance ahead of notch, normalized by the notch-root radius



Toughness of Dentin – Effect of Orientation

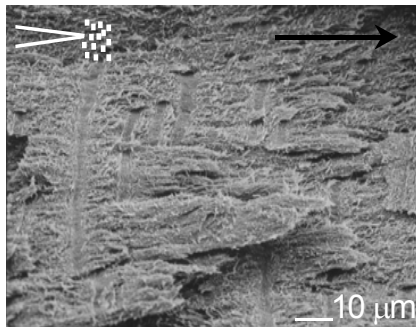


Anisotropy in Toughness in Dentin

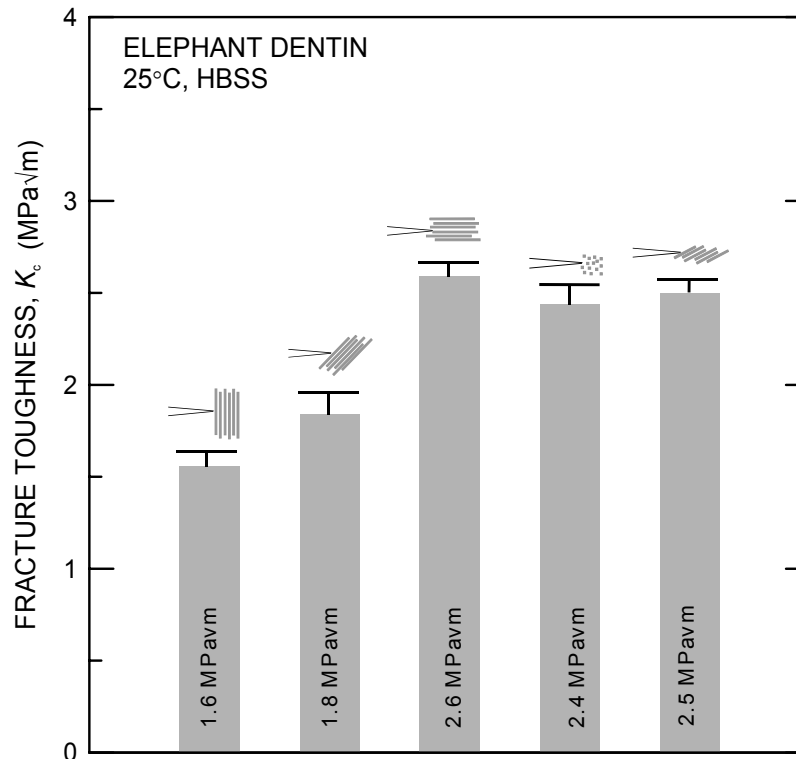


perpendicular orientation

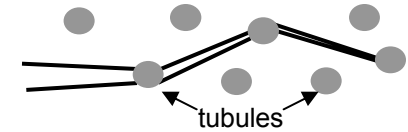
**Toughness
anisotropic with
tubule orientation**



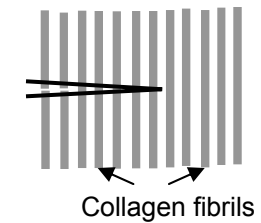
anti-plane parallel orientation



Toughening Mechanisms

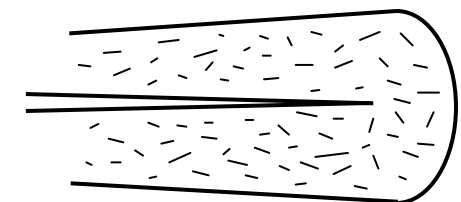


crack deflection



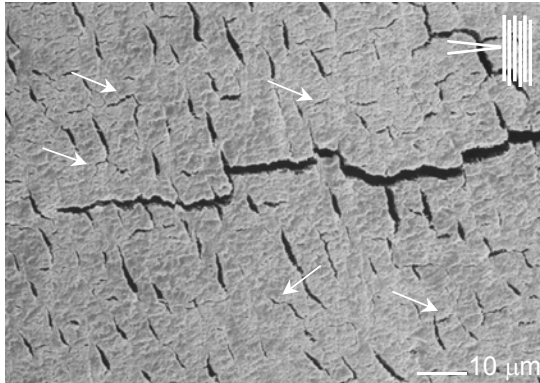
fibril bridging

uncracked ligament bridging



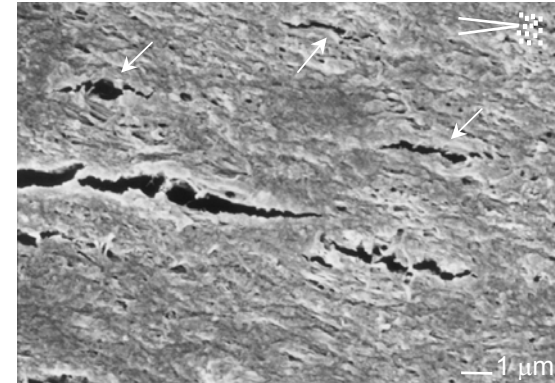
microcracking

Toughening Mechanisms in Dentin



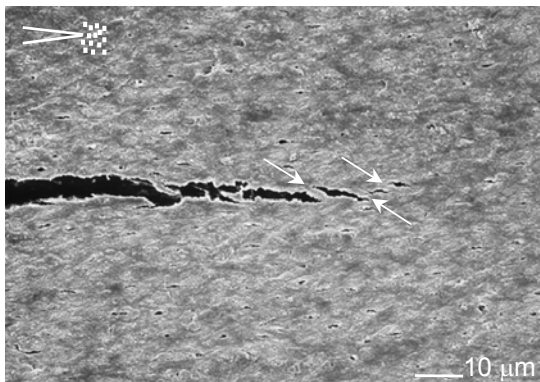
← crack growth direction

Crack Deflection
(very localized)



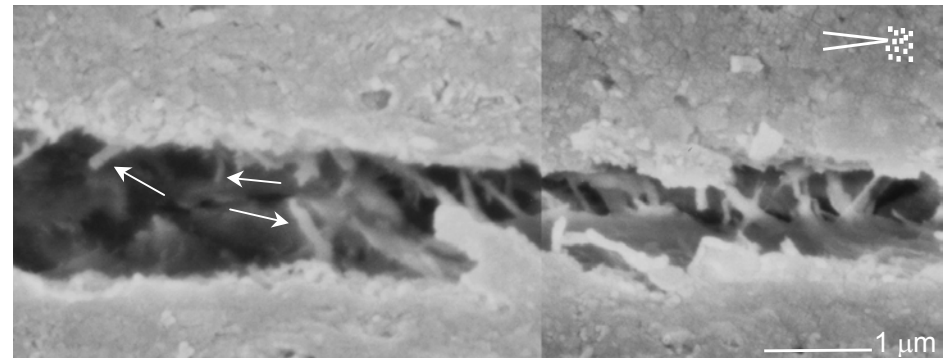
crack growth direction →

Microcracking
($K_{mic} \sim 0.3 \text{ MPa}\sqrt{\text{m}}$)



crack growth direction →

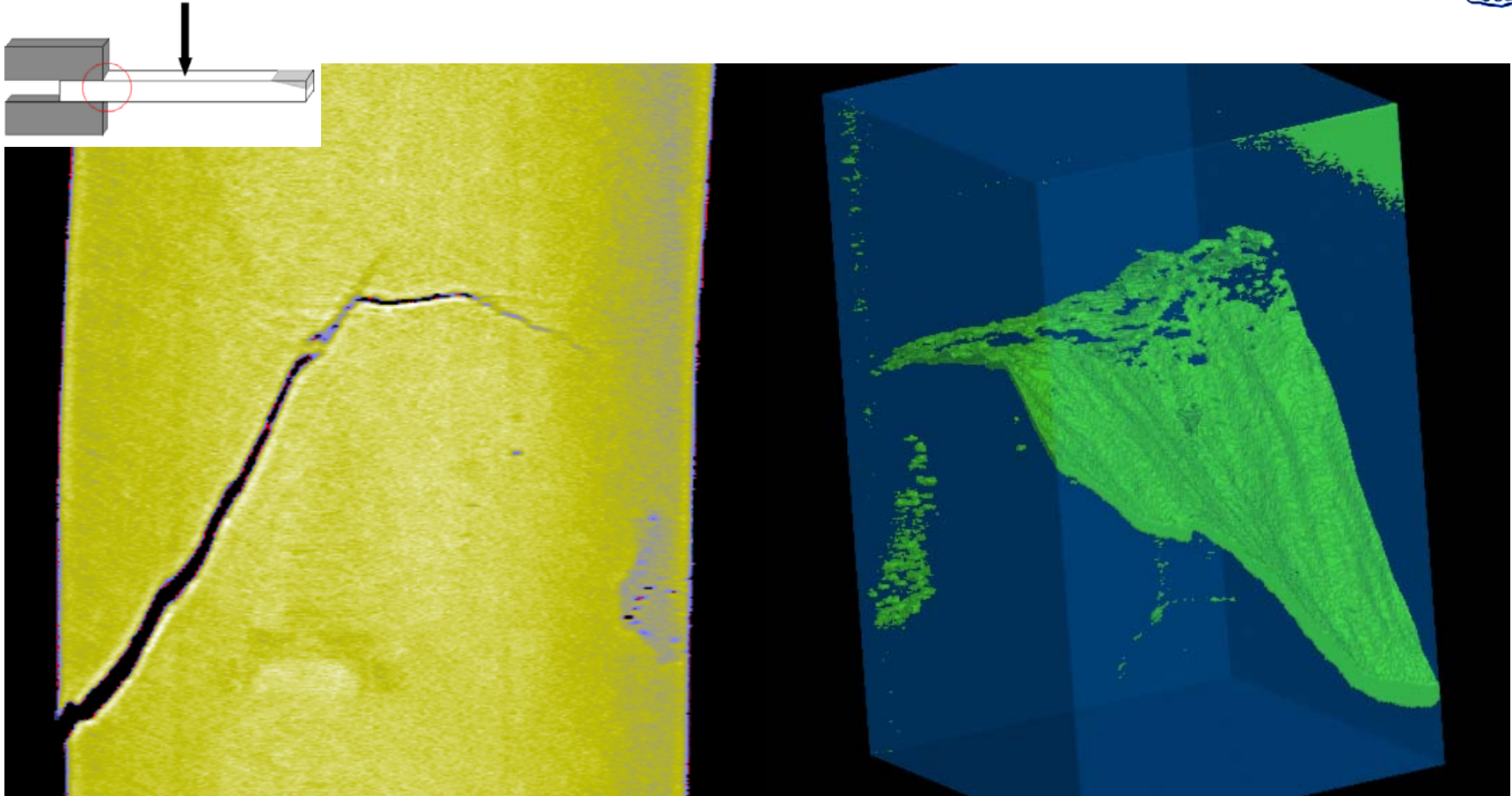
Uncracked Ligament Bridging
($K_b^{ul} \sim 0.1\text{-}0.4 \text{ MPa}\sqrt{\text{m}}$)



crack growth direction →

Collagen Fibril Bridging
($K_b^f < 0.1 \text{ MPa}\sqrt{\text{m}}$)

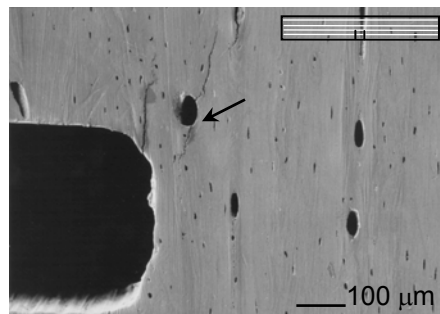
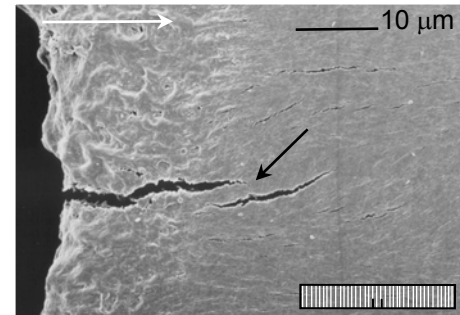
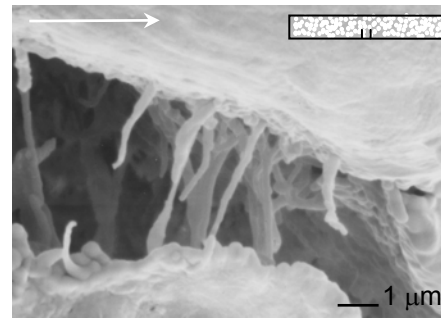
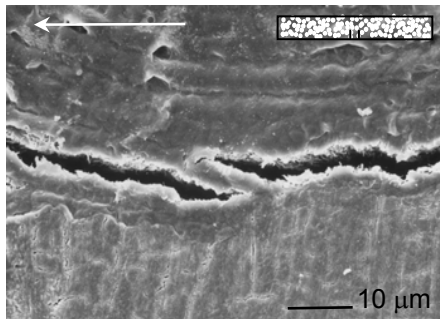
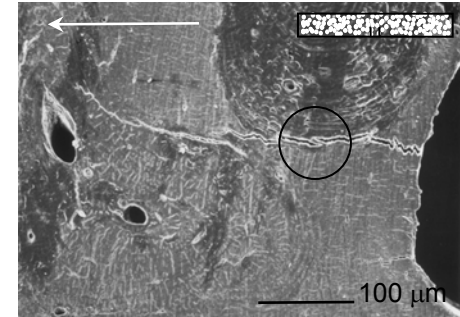
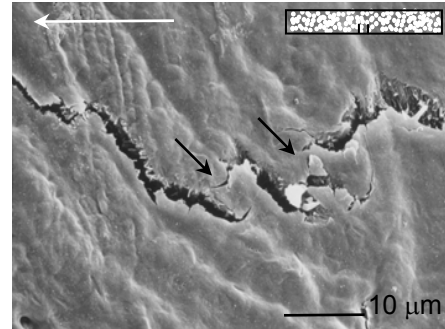
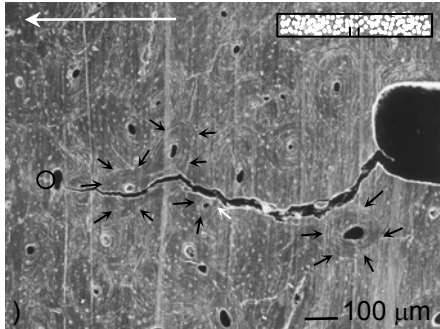
X-Ray Computed Tomography



- clear three-dimensional evidence of uncracked ligament bridging

imaged at the Stanford Synchrotron Radiation Laboratory - SSRL, Stanford Linear Accelerator Center - SLAC

Toughening Mechanisms in Bone



Uncracked Ligament Bridging

$$K_b^{ul} \sim 0.3 \text{ MPa}\sqrt{\text{m}} \quad (\text{in-plane longitudinal})$$

Fibril Bridging

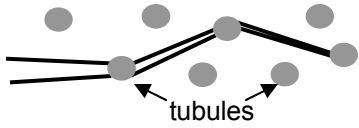
$$K_b^f \sim 0.07 \text{ MPa}\sqrt{\text{m}} \quad (\text{anti-plane longitudinal})$$

Crack Deflection

$$K_d \sim 2.7 \text{ MPa}\sqrt{\text{m}} \quad (\text{transverse})$$

Toughening Mechanisms

Crack Deflection



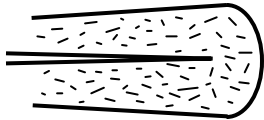
$$k_1(\alpha) = c_{11}(\alpha) K_I + c_{12}(\alpha) K_{II}$$

$$k_2(\alpha) = c_{21}(\alpha) K_I + c_{22}(\alpha) K_{II}$$

$$K_d = (k_{12} + k_{22})^{1/2}$$

(Bilby *et al.*, 1978; Cottrell & Rice, 1980)

Microcracking



$$K_{mic} = 0.22 \varepsilon_m E' f_m l_m^{1/2} + \beta f_m K_c$$

(Evans & Fu, 1985; Hutchinson, 1987)

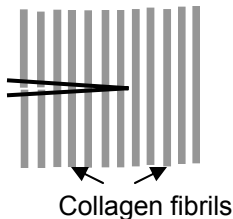
Uncracked Ligament Bridging



$$K_b^{ul} = -f_{ul} K_I [(1 + l_u / rb)^{1/2} - 1] / [1 - f_{ul} + f_{ul} (1 + l_u / rb)^{1/2}]$$

(Shang & Ritchie, 1989)

Collagen Fibril Bridging



$$K_b^f = 2 \sigma_b f_f (2 l_f / \pi)^{-1/2}$$

(Evans & McMeeking, 1986)

Dentin

very localized
(perpendicular)

0.3 MPa√m
(both)

0.1-0.4 MPa√m
(parallel)

<0.1 MPa√m
(parallel)

Bone

2.7 MPa√m
(transverse)

-

0.3 MPa√m
(in-plane long.)

0.07 MPa√m
(anti-plane long.)

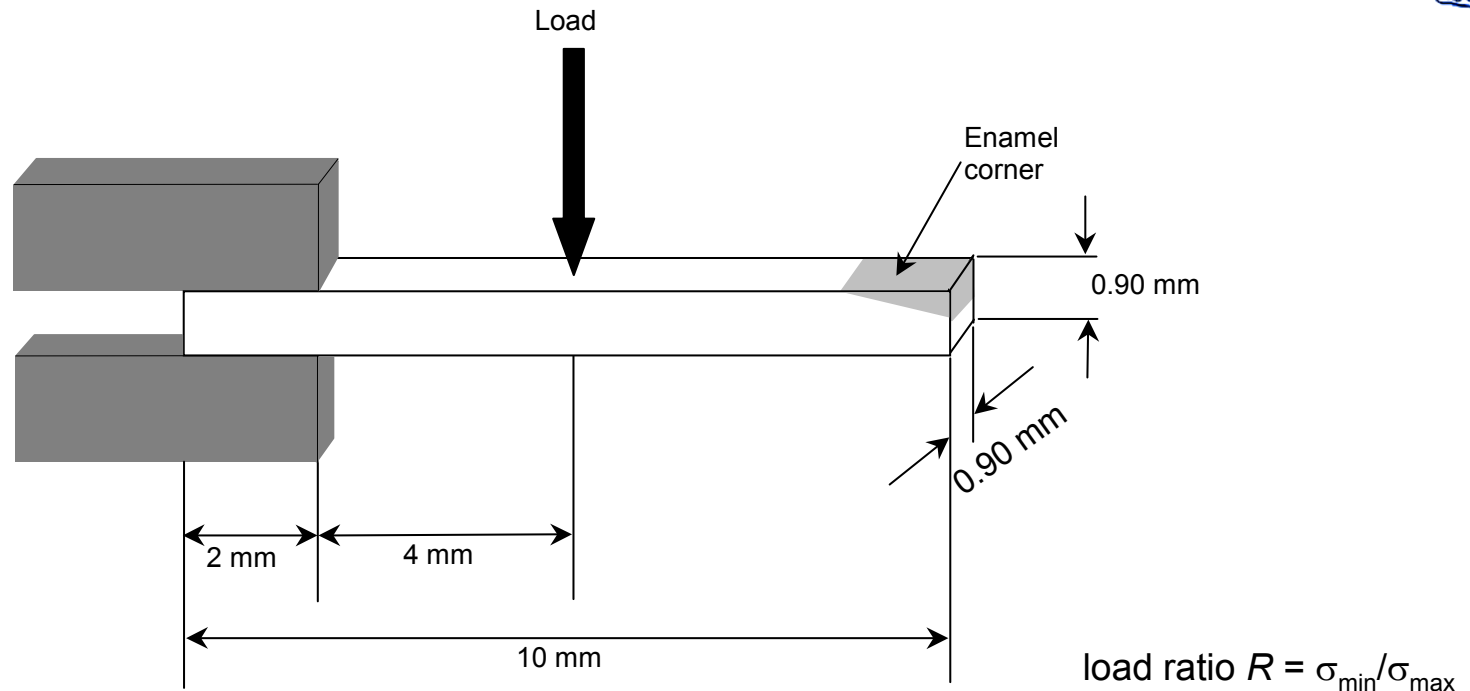


Fatigue of Dentin



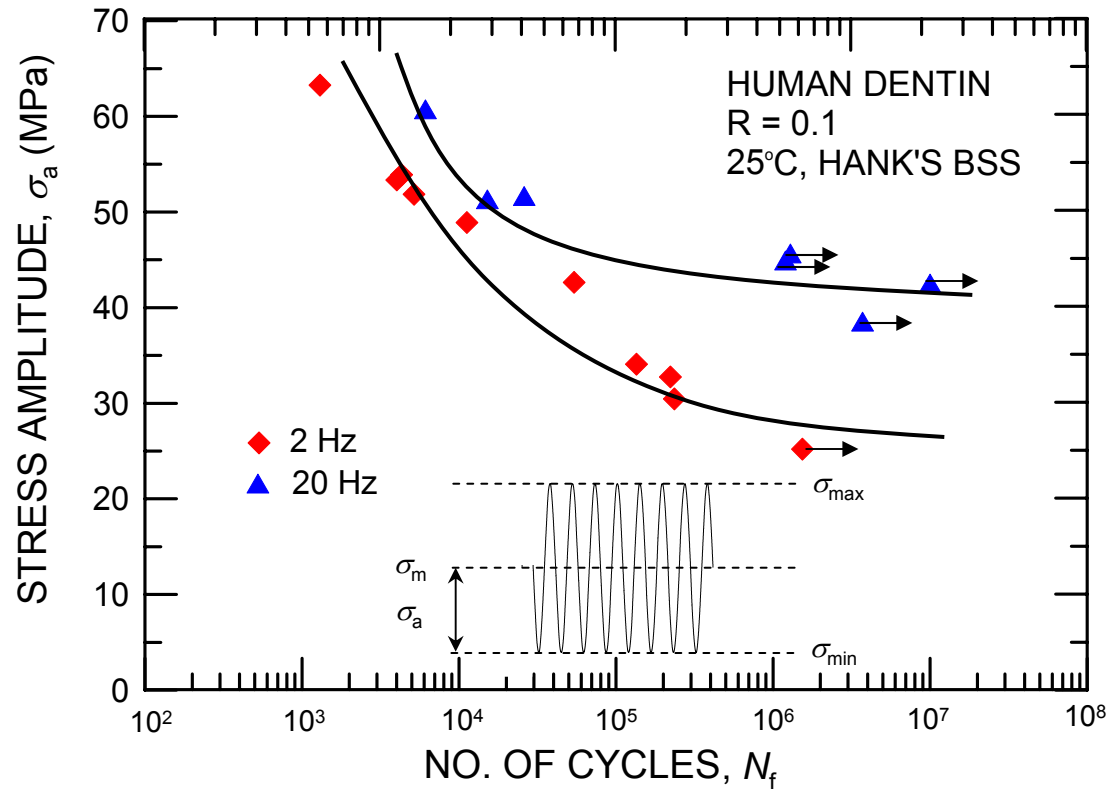
- Tonami *et al.*, (1997)
 - 10^5 -cycle tensile fatigue strength measured for *bovine* dentin
 - Fatigue strength of 47-51 MPa found: lower value for older animals
 - Tests only over narrow range of purely tensile load ratios, $R \sim 0.15$ -0.25
 - tests conducted at 37°C in water; demineralization concerns
 - test duration too short; typical teeth loaded more than 10^6 times annually
- Arola *et al.*, (2002)
 - preliminary crack-growth data for *bovine* dentin
 - zero-tensile ($R \sim 0$) cycling at 25 Hz in a saline bath at 21°C
 - rates of fatigue-crack growth highest perpendicular to the tubules
- Absolutely no data on human dentin

Stress-Life (S/N) Approach



- cantilever-beam geometry
- all tests in conducted in Hank's Balanced Salt Solution (HBSS)
- all tests performed on an ELF[®] 3200 series acoustic testing machine (EnduraTEC Inc., Minnetonka, MN)
- three frequencies, 2 Hz, 10 Hz, 20 Hz; wide range of load ratios, $R = -1$ to 0.5

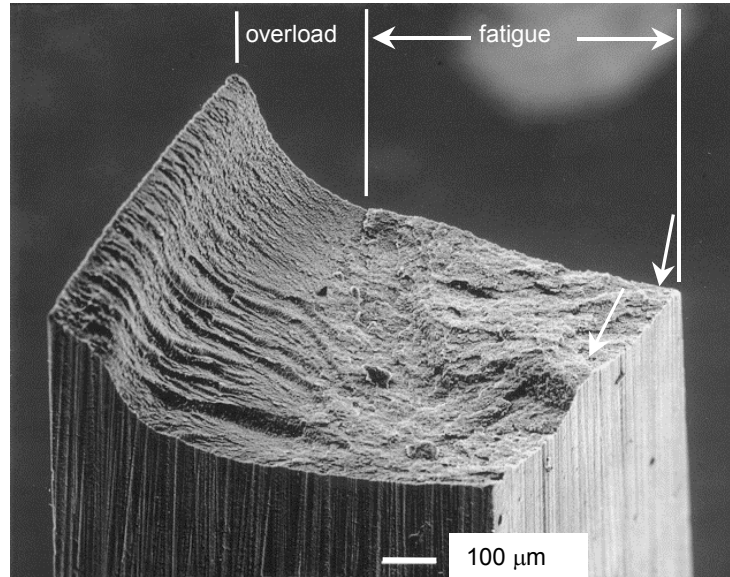
S/N Results on Human Dentin



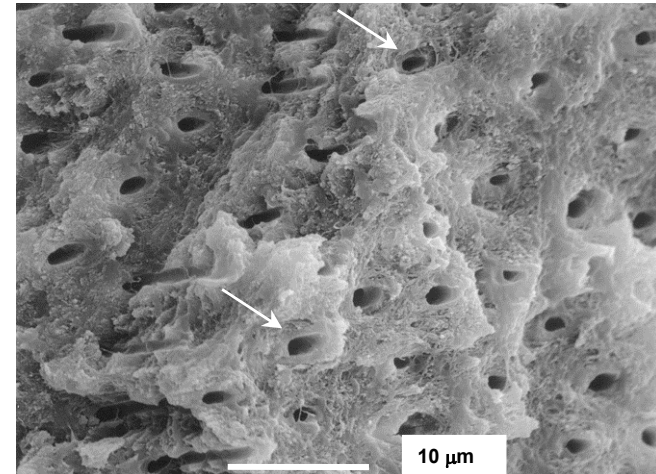
- clear evidence of a susceptibility of human dentin to fatigue
- “metal-like” fatigue S/N behavior with frequency-dependent fatigue limit at 10^6 - 10^7 cycles of ~25 and 45 MPa
- fatigue lives, in terms of cycles to failure are shorter at lower frequency

Fractography

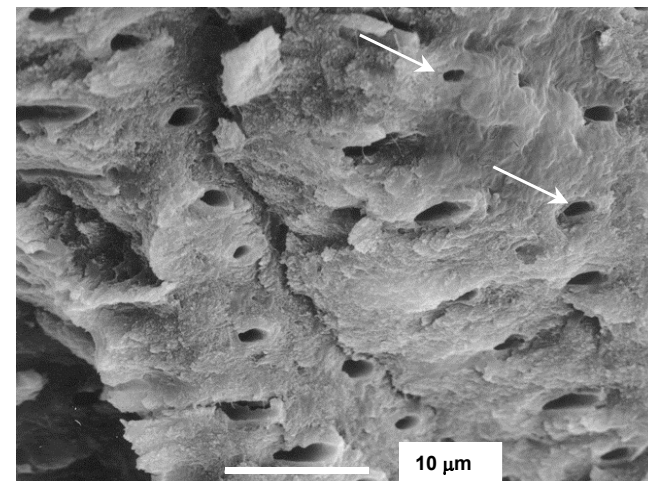
Fatigue surface



- Morphology of the fracture surfaces during fatigue-crack propagation essentially identical to overload (catastrophic) failure

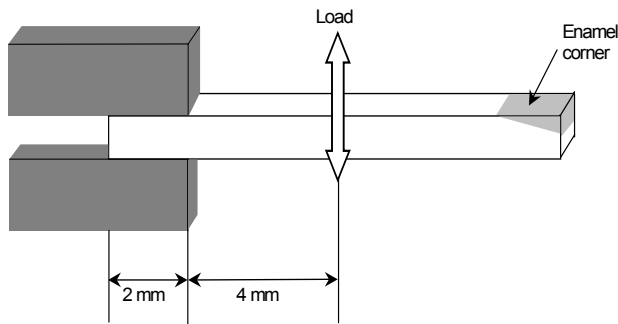
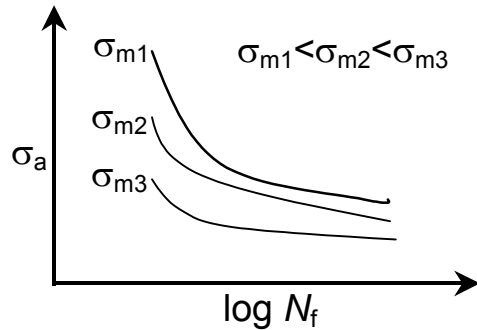


Crack Growth Direction →

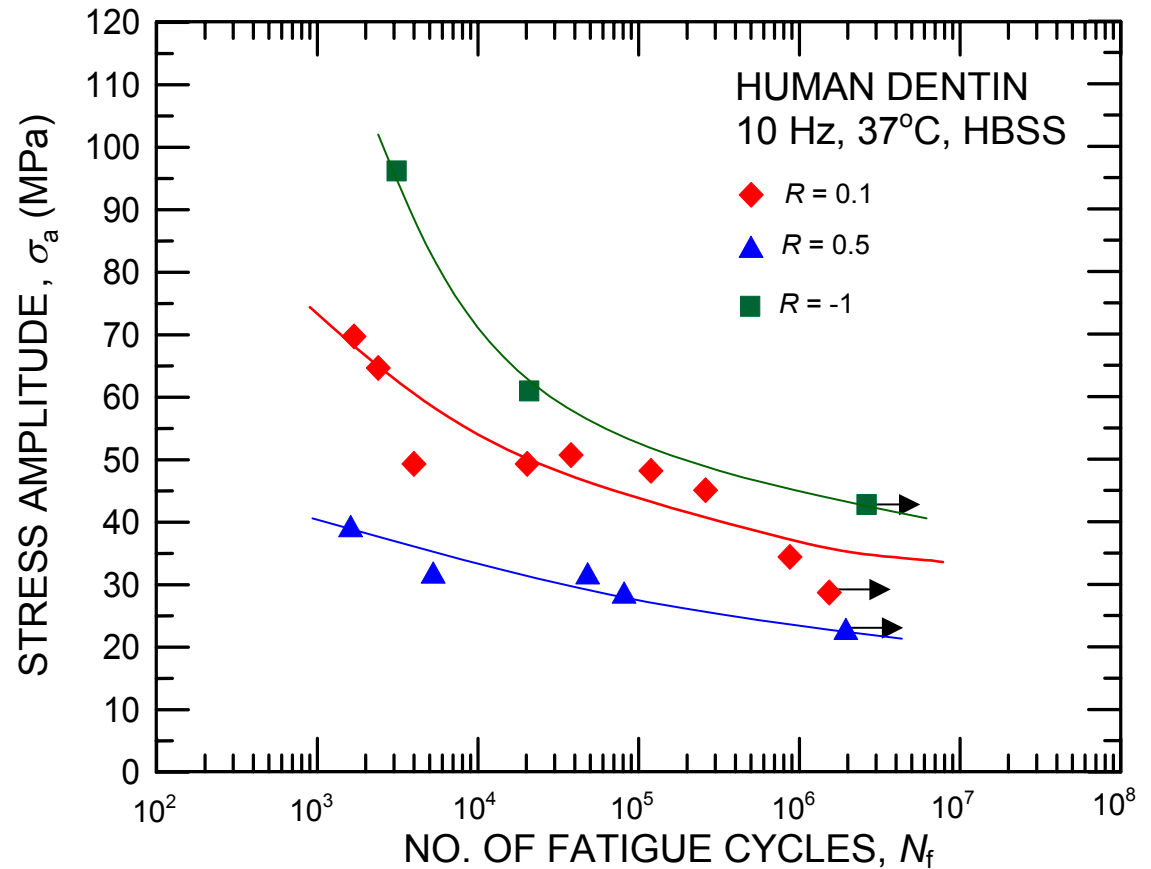


Overload surface

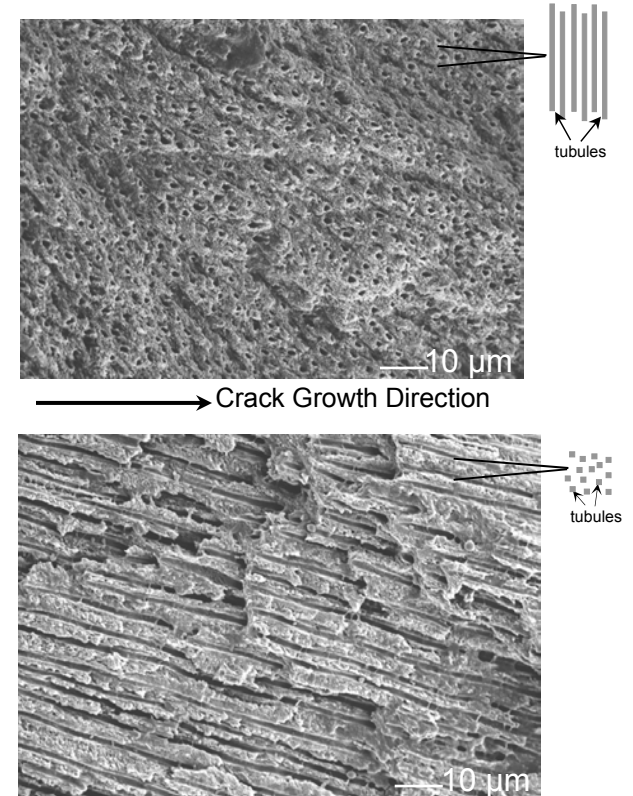
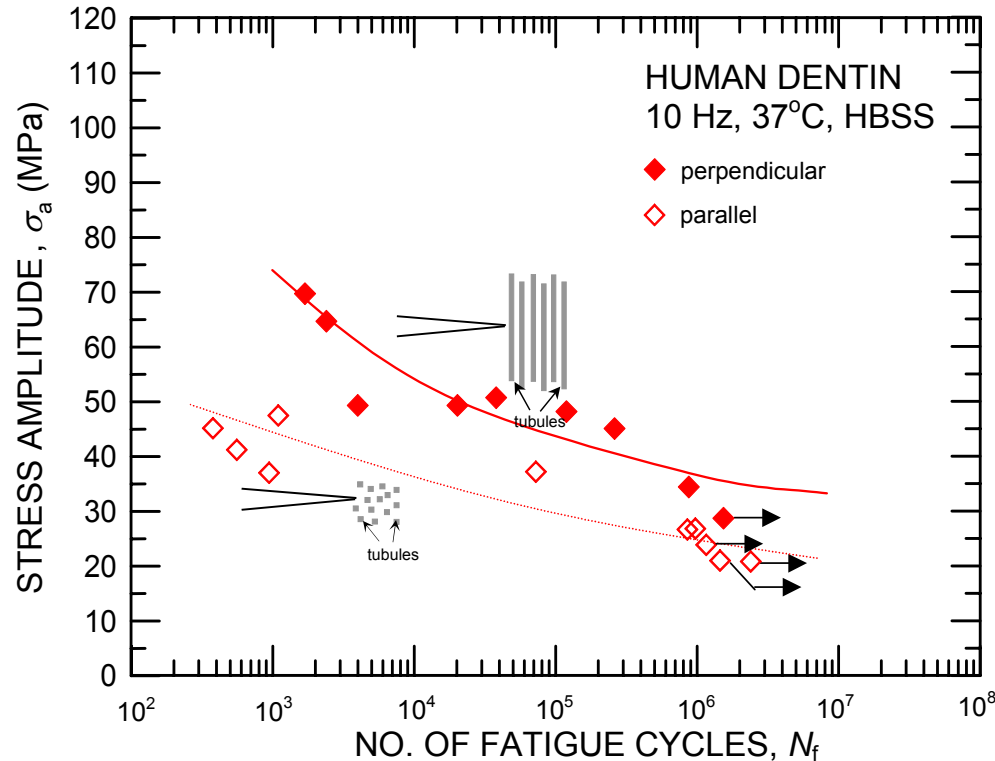
Effect of Mean Stress (Load Ratio)



- cantilever bending
- R ratios: 0.1, 0.5 and -1
- 10 Hz, 37°C, HBSS

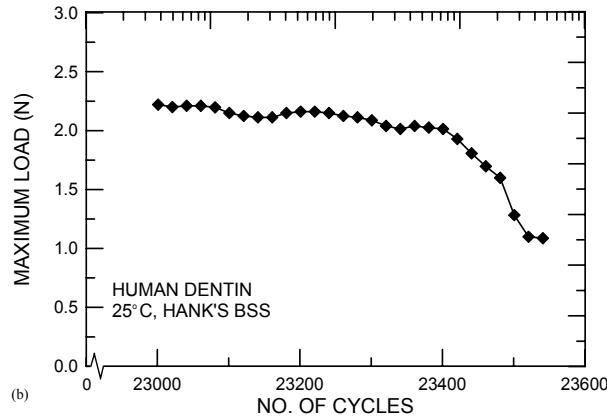


Orientation Effects

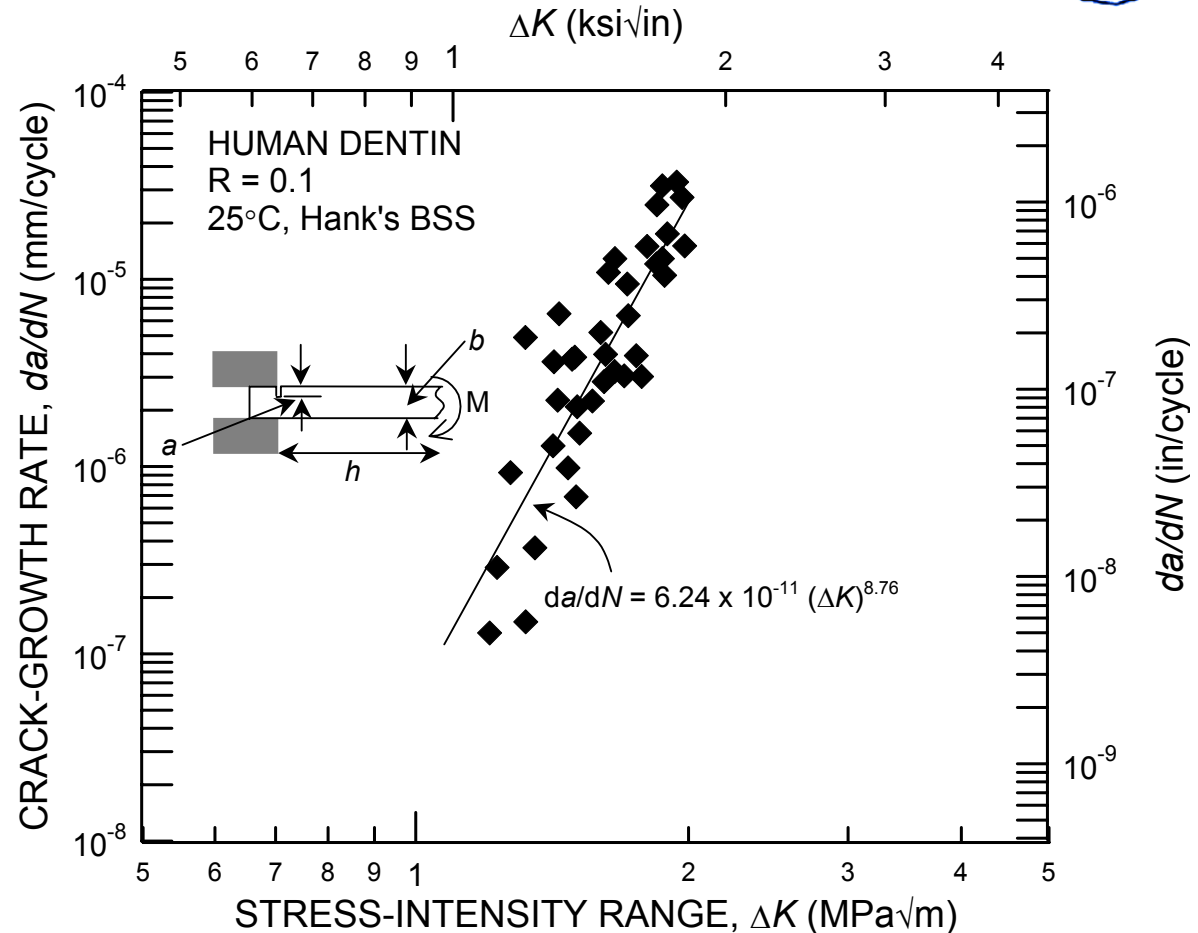


- microstructure affects both LCF and HCF behavior
- lower fatigue limits for *parallel*, as compared to *perpendicular*, orientation
- orientation effect in fatigue contrary to that seen for toughness

Fatigue-Crack Growth in Human Dentin



- decay in stiffness used to estimate crack lengths



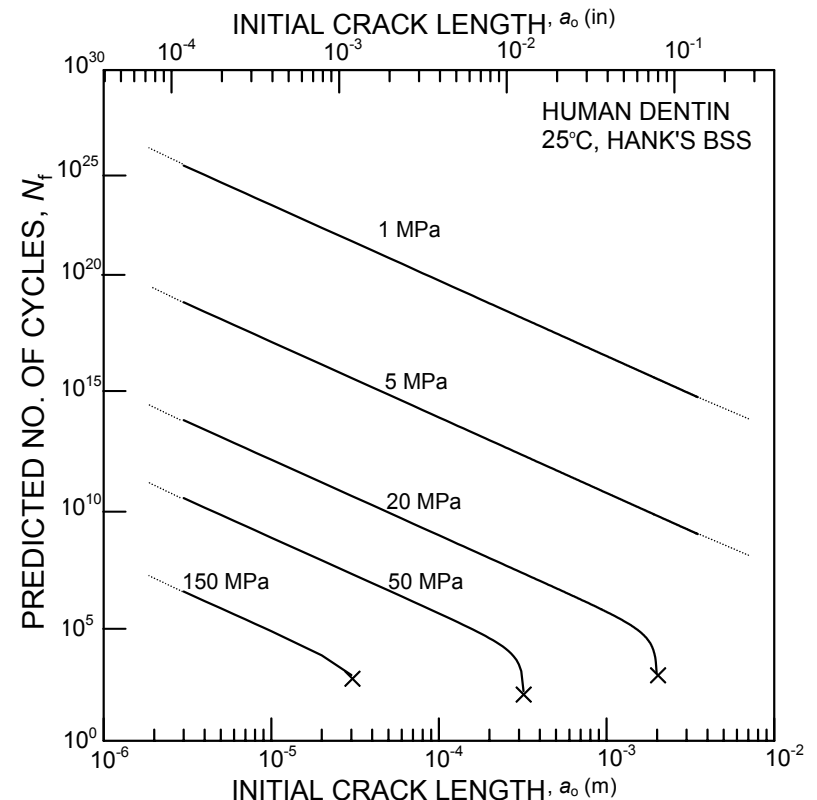
- Paris power-law relationship, $da/dN = C \Delta K^m$, where exponent $m \sim 8.76$
- Estimated fatigue threshold, $\Delta K_{TH} \sim 1.06 \text{ MPa}\sqrt{m}$, $\sim 60\%$ of the fracture toughness

Damage-Tolerant Lifetime Prediction

- Integrating the Paris equation, from an initial, a_o , to final, a_c , crack size:

$$N_f = 2 (f(a/b)\Delta\sigma_{app})^{-m} (m-2)^{-1} C^{-1} \pi^{-m/2} [a_o^{1-m/2} - a_c^{1-m/2}]$$

- for initial flaw size, $a_o \sim 100 \mu\text{m}$, projected life at $\sigma_{app} \sim 20 \text{ MPa}$ over a billion cycles
- for a $600 \mu\text{m}$ flaw, projected life drops to ~ 3.6 million cycles, or 3 to 4 years
- for a $900 \mu\text{m}$ flaw, projected life as low as a few months
- for *in vivo* stresses of 5-20 MPa, small flaws in teeth, $\sim 250 \mu\text{m}$, will not radically affect their structural integrity, as predicted fatigue lifetimes exceed patient lifetimes



Summary

- First accurate fracture toughness of human dentin measured.
- Critical fracture event in dentin consistent with a *strain-based* criterion.
- Effect of orientation on toughness defined; lowest toughness measured for fracture perpendicular to dentinal tubules.
- Toughness in dentin arises from extrinsic toughening mechanisms: collagen fibril and uncracked ligament bridging, microcracking, crack deflection.
- Human dentin shown to be susceptible to fatigue failure.
- “Metal-like” *S/N* behavior seen, sensitive to both frequency and mean stress, with a 10^6 - 10^7 cycle fatigue limit of 25-45 MPa.
- Rudimentary life-prediction analyses indicates that flaws of up to 250 μm in size will not radically affect structural integrity under typical physiological loads.